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Engineering a High-Selectivity PVDF Hollow-Fiber Membrane for Cesium Removal



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ABSTRACT

In this study, a copper ferrocyanide/silica/polyvinylidene fluoride (CuFC/SiO₂/PVDF) hollow-fiber composite membrane was successfully synthesized through a facile and effective crosslinking strategy. The PVDF hollow-fiber membrane with embedded SiO₂ was used to fix the dispersion of CuFC nanoparticles for cesium (Cs) removal. The surface morphology and chemical composition of the composite membrane were analyzed using scanning electron microscopy and X-ray photoelectron spectroscopy (XPS). The composite membrane showed a high Cs rejection rate and membrane flux at the three layers of CuFC and 0.5% SiO₂, and its Cs rejection rate was not affected by variation in the pH (pH = 4–10). The modified membrane could be effectively regenerated many times using ammonium nitrate (NH₄NO₃). The Cs selectivity performance was verified by an efficient Cs rejection rate (76.25% and 88.67% in 8 h) in a solution of 100 μ g·L⁻¹ of Cs with 1 mmol·L⁻¹ of competing cations (K⁺ and Na⁺). The CuFC/SiO₂/PVDF hollow-fiber composite membrane showed a particularly superior removal performance (greater than 90%) in natural surface water and simulated water with a low Cs concentration. Therefore, the CuFC/SiO₂/PVDF hollow-fiber composite membrane can be used directly in engineering applications for the remediation of radioactive Cs-contaminated water.

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1. Introduction

The release of large amounts of radionuclides into the aquatic environment has attracted worldwide attention after the Fukushima Daiichi nuclear power plant accident in 2011 [1,2]. Among such radionuclides, the concentration of cesium (¹³⁷Cs) is very high because of the long half-life (30.1 years) and high mobility of this element; thus, Cs poses a particular threat to environmental safety and human health [3]. Although there have been many studies on effective removal techniques for trace radionuclides, monovalent Cs removal still faces great challenges due to the highly active biochemical characteristics of Cs, which are similar to those of potassium [4]. Many Cs removal methods have been reported, including adsorption, membrane technology, distillation, and chemical precipitation [5–9]. Of these methods, adsorption is one of the most effective removal techniques for Cs.

Various types of Cs adsorbents including molybdophosphate, metallic oxides, zeolites, carbon, and other clay minerals have been extensively studied [4,10–14]. However, these absorbents have a low selectivity for removing Cs from water. Transition metal ferrocyanides (Cu, Fe, Zn, and Ni) are extensively used as absorbents due to their high selectivity for Cs and low cost [15–19]. These absorbents always have a lattice spacing size of about 0.32 nm, which is similar to that of the hydrated ion of Cs [20]. In particular, copper ferrocyanide (CuFC) has shown excellent Cs sorption capacity and chemical stability, and has been used to selectively separate Cs from contaminated wastewater [3,15,21–23]. However, CuFC is commonly available in the form of fine particles that are difficult to separate and collect, which limits its practical application [24].

In recent decades, supporting materials with magnetism or high surface areas have been selected to immobilize CuFC [15,22,25,26]. For example, CuFC-type particles can be loaded onto silica (SiO₂) to

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improve their mechanical properties, which results in a high Cs rejection rate [27]. The problem of the difficult separation and recovery of the adsorbents has not been solved by fixing them onto the surface of particles. Chen et al. [28] tried to fix transition metal ferrocyanides directly onto a non-woven fabric to solve this problem. To remove heavy metal ions, Efome et al. [29-31] fixed metalorganic framework adsorption materials to a membrane using electrostatic spinning technology in order to effectively solve the problem of nano-materials fixation. However, the efficiency of the adsorption materials may decrease through internal fixation. Recently, transition metal ferrocyanide nanolayers on membranes were engineered to remove Cs from water [32–36]. However, the adsorbent particles directly loaded on the membrane surface blocked the membrane's pores and affected the membrane's filtration efficiency. A substrate with a binding agent can be used in membrane filtration with an acceptable flux and a minimal pressure drop [10,37]. Ding et al. [10] demonstrated an absorbentbead structured membrane that was functionalized to effectively eliminate Cs through a filtration adsorption method. Nevertheless, a chemical bonding method can fix the particle substrate on the surface of a membrane more firmly than anchoring through a physical deposition method. Qin et al. [38] reported that the use of chemical bonding to load TiO₂ nanoparticles (NPs) onto a polyvinylidene fluoride (PVDF) membrane greatly improved the membrane flux and increased the stability of the composite membrane. As far as we know, the chemical bonding of transition-metal ferrocyanide-coated NPs onto a hollow-fiber membrane surface for the removal of Cs in water has not been well documented.

In the present work, we synthesized CuFC/SiO₂-incorporated PVDF (CuFC/SiO₂/PVDF) hollow-fiber composite membranes for the effective removal of Cs in water. The physicochemical characteristics of the composite membranes were analyzed and their Cs rejection abilities were studied.

2. Material and methods

2.1. Chemicals and reagents

Non-radioactive cesium nitrate was used as an alternative to 137 Cs due to its similar chemical properties. Tetrabutylammonium fluoride (TBAF, 98%) and trimesoyl chloride (TMC, 98%) were supplied by Sigma-Aldrich. SiO₂ NPs modified by amino groups (w/v: 2.5%; particle size: 300 nm) were purchased from Aladdin. Sodium ferrocyanide (Na₄[Fe(CN)₆]·10H₂O) and other reagents used in this work were provided by Sinopharm. Ultrapure water prepared by the Milli-Q IQ7000 (Millipore, USA) water purification system was used in this study.

2.2. Membrane surface modification

A PVDF hollow-fiber membrane (OriginWater, U100 MF, 0.1- $1\,\mu m$) was chosen for this study and was further modified by a reported method developed with a minor modification [38]. First, the two terminals of the hollow-fiber membranes were sealed with epoxy resin for 24 h; the membranes were then washed with water for 24 h, and then dried at room temperature after washing with ethanol for 1 h. The membranes were then further modified, as follows: ① Pristine PVDF membrane was immersed in 1 mol·L⁻¹ potassium hydroxide (KOH) solution with $5 \text{ g} \cdot \text{L}^{-1}$ TBAF for 60 min at 45 °C, and then dipped into 1 mol·L⁻¹ sodium hydrogen sulfite (NaHSO₃) aqueous solution with H₂SO₄ for 1 h at 45 °C; (2) the treated membrane was then immersed by 0.8 wt% TMC hexane solution; ③ the treated membrane was dipped into SiO₂ suspension with a mass concentration of 0.05% and 0.5%. respectively, for 60 min at 100 r·min⁻¹ and 25 °C. Next, the membrane was heated at 70 °C for 5 min to improve the grafting reaction. Finally, the membrane was washed and marked as SiO₂/PVDF hollow-fiber composite membrane (Fig. 1).

2.3. CuFC/SiO₂/PVDF hollow-fiber composite membrane preparation

The modified membranes were dipped into 50 mL CuCl₂ (0.5 mol·L⁻¹) and placed in a shaker with a shaking speed of 120 r·min⁻¹ for 2 h at 25 °C. The membranes were then transferred into 50 mL of 0.5 mol·L⁻¹ Na₄[Fe(CN)₆] solution and were agitated at 150 r·min⁻¹ for 4 h at 25 °C. The final CuFC-modified membranes were washed many times to elute any residual solution. The loading process of CuFC was repeated one to three times to grow the crystal. Next, ultrapure water was used to wash the modified membranes. The prepared membranes were dried at 40 °C and then stored in ultrapure water (Fig. 1).

2.4. Membrane characterization

The surface morphology of the membranes was characterized by scanning electron microscopy, and the element composition of the membrane surface was analyzed by X-ray photoelectron spectroscopy (XPS). The membrane surface was evaluated for the binding performance of the CuFC and SiO₂ NPs via an ultrasonic test for 2 min and then tested again for another 2 min. In the end, the weight and surface morphology of the composite membrane before and after the treatment were determined. Membrane regeneration was carried out by soaking the membrane in a solution of 5 mol·L⁻¹ ammonium nitrate (NH₄NO₃) at 120 r·min⁻¹ for 24 h at 25 °C.

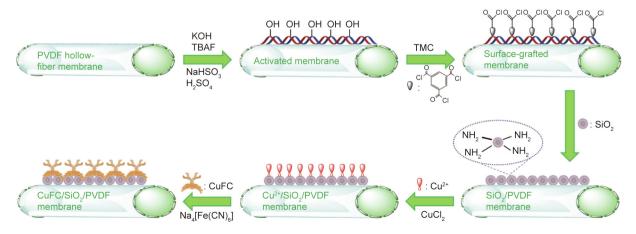


Fig. 1. Schematic diagram of CuFC/SiO₂/PVDF hollow-fiber composite membrane preparation.

2.5. Membrane filtration experiments

Cs solutions of 100 μ g·L⁻¹ were used to conduct the filtration tests. NaOH or HCl solution was used to maintain the solution at pH = 7 ± 0.1. One membrane filtration system (Fig. 2) was used to assess the Cs rejection ability and water permeability of the membrane at 90 kPa. The effective membrane area was 12.5 cm². After 1 h of water filtration, the membrane flux was tested and the permeate samples were analyzed.

The effect of the organic matter (5.0 mg·L⁻¹ humic acid, HA) and competing cations (1 mmol·L⁻¹ K⁺, Na⁺) on the Cs removal was explored. The physicochemical properties of natural surface water (SW) were tested after filtering through 0.45 µm film; the results are displayed in Table 1. Next, 100 µg·L⁻¹ Cs solutions in SW and HA solution were used to conduct the filtration experiments. An inductively coupled plasma mass spectrometer was used to test the Cs concentration. The concentrations of cations and anions were analyzed using an inductively coupled plasma atomic emission spectrometer and ion chromatography, respectively.

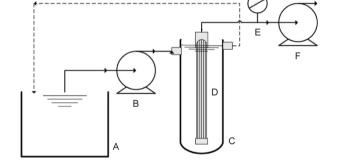


Fig. 2. Schematic diagram of the membrane filtration system. A: feed tank; B: pump; C: membrane element; D: membrane; E: pressure gauge; F: pump.

Table 1

The properties of the SW collected	from Wu River (Guizhou, China).
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3. Results and discussion

3.1. Properties of PVDF hollow-fiber membranes

The amino-modified SiO₂ NPs were bound with the reactive groups (-COCl) of the pristine PVDF membrane surface, which was formed by pretreating in an alkaline solution and TMC hexane media [38]. The CuFC was then loaded onto the SiO₂ NP surface. As shown in Fig. 1, dehydrofluorination and nucleophilic addition were the two main modification steps. Treatment with KOH solution facilitated the formation of unsaturated double bonds in the pristine PVDF membrane, which was followed by the formation of hydroxyl groups to induce a nucleophilic addition reaction on the polymer chains. XPS was used to test the modification characteristics; the results are shown in Fig. 3. A dramatic change in the XPS wide spectra was seen in the SiO₂/PVDF hollow-fiber composite membranes but not in the pristine membrane. The ratio of oxygen atoms increased, indicating that oxygen-containing groups had been introduced onto the surface of the membrane [38]. Two more peaks of Si 2s and Si 2p appeared in addition to the peaks of C 1s, O 1s, and F 1s, which verified that successful binding of SiO₂ on the PVDF membrane had occurred. A high content of SiO₂ particles facilitated the contact with the pretreated PVDF membrane and promoted the loading of SiO₂ onto the membrane surface through binding with the active group. Furthermore, as shown in Fig. 3, an Fe 2p peak (708.6 eV) and a Cu 2p peak (932.7 eV) appeared on the composite membrane, respectively, in accordance with the presence of $Fe(CN)_6^{4-}$ and Cu [39,40], respectively, demonstrating that CuFC was successfully loaded onto the membrane.

The surface morphologies of the PVDF membranes were characterized; the results are shown in Fig. 4. The pristine membrane showed the typical structure of a microfiltration microfiltration membrane, having a porous skin layer. The results also demonstrated that the amount of SiO₂ NPs increased with the initial concentration used for loading SiO₂ (Figs. 4(b) and (c)). The surface of the CuFC/SiO₂/PVDF (0.05%) showed aggregates of porous platelets (Fig. 4(d)), indicating that CuFC was successfully loaded onto the

pH	Concentration								
	DOM (mg·L ⁻¹)	Cs^+ ($\mu g \cdot L^{-1}$)	Na ⁺ (mg·L ⁻¹)	K^+ (mg·L ⁻¹)	Ca ²⁺ (mg·L ⁻¹)	Mg^{2+} (mg·L ⁻¹)	Cl^- (mg·L ⁻¹)	NO_3^- (mg·L ⁻¹)	SO_4^{2-} (mg·L ⁻¹)
7.81	2.37	0.91	4.35	2.79	44.79	13.46	4.74	3.16	45.93

DOM: dissolved organic matter.

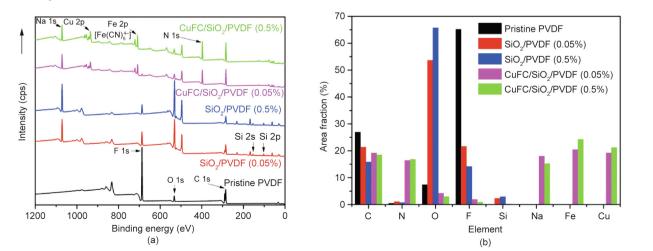


Fig. 3. (a) Elemental composition of membrane surfaces by XPS; (b) area fractions of elements on the membrane surfaces. 0.05% and 0.5% refer to the mass concentrations of SiO₂. Cps: counts per second.

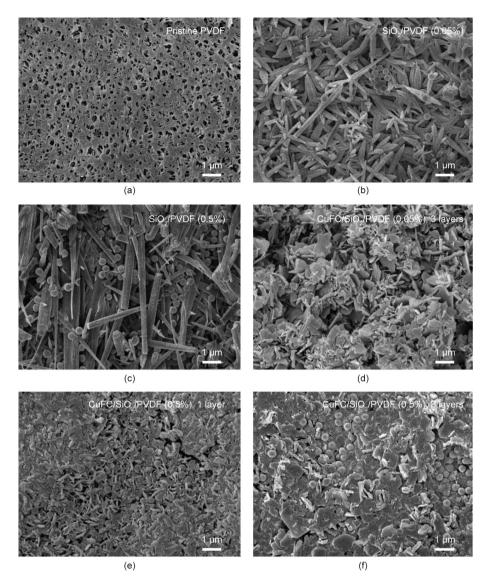


Fig. 4. Surface morphology of the PVDF membranes. (a) Pristine PVDF membrane; (b) and (c) SiO₂/PVDF membranes; (d-f) CuFC/SiO₂/PVDF membranes.

membrane surface [41]. In addition, there was a formed selective CuFC layer (one layer and three layers) on the surface of the composite membrane (Figs. 4(e) and (f)), which might be due to the SiO_2 layer being stabilized on the surface of the membrane.

The Cs rejection rate and flux of these membranes were tested; the results are shown in Table 2. It can be seen that the rejection rate increased and the flux decreased with an increase of the loaded layer. At a concentration of 0.05% SiO₂, the rejection rate of the composite membrane with three layers of CuFC was higher than 90%, even with decreasing membrane flux. In order to achieve the highest rejection rates, 0.5% SiO₂-loaded composite membranes were selected in the following experiments.

3.2. Binding stability of modified membrane

As shown in Figs. 4(f) and 5, there was almost no morphological change on the hollow-fiber composite membrane surface before and after physical treatment. It was also demonstrated that the fixation ability of the SiO_2 NPs for CuFC effectively inhibited delamination or peeling between the membrane surface and the CuFC layer. Furthermore, the membrane weight decreased by just 0.2 mg after the physical treatment of the membrane—an amount that could be ignored. Thus, the results of the weight measurements and surface morphology indicated that the binding between the PVDF membrane and the CuFC NPs was strong.

Table 2

Rejection rate and flux of composite membranes with different layers of CuFC and different concentrations of SiO₂ (Cs: 100 µg·L⁻¹; pH = 7).

CuFC load layer	Concentration of SiO ₂ (%)	Flux $(L \cdot (m \cdot h \cdot k Pa)^{-1})$	Rejection rate after 1 h (%)	Rejection rate after 6 h (%)
1	0.05	1.61	70.25	49.36
3	0.05	0.30	94.20	89.68
1	0.5	2.92	87.45	78.22
3	0.5	0.49	99.82	94.64

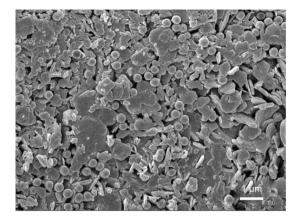


Fig. 5. Surface morphology of the composite membrane after physical treatment.

3.3. Regeneration of modified membrane

It is a major challenge to establish membrane treatment methods that can recover after being used several times. To evaluate membrane regeneration, NH₄NO₃ solution was used to regenerate the filtered composite membrane [42,43]. The Cs rejection rate of the regenerated membrane after being used for 18 h was evaluated. As shown in Fig. 6, the rejection rate of the composite membrane decreased with increasing treatment time. The membrane regeneration was carried out after 18 h. After two cycles of NH₄NO₃ regeneration, the Cs rejection rate was still greater than 98%. Egorin et al. [42] reported that more than 63% of Cs desorption could be achieved from CuFC adsorbent in seawater after regeneration with 5 mol·L⁻¹ NH₄NO₃ solution. Thus, the composite membrane can be regenerated efficiently by NH₄NO₃ solution many times, giving it potential for practical applications.

3.4. Effect of initial pH

The Cs rejection rate may be affected by the pH of the feed solution; therefore, a series of experiments was carried out over a pH range from acidity to alkalinity. As shown in Fig. 7, the membranes exhibited the maximal rejection rate at pH = 7; the rejection rate decreased at pH = 4 and at a pH higher than 7 (Fig. 7). The phenomenon of decreased rejection rate at low pH might be caused by the competing adsorption of H⁺ and Cs onto the CuFC/SiO₂/PVDF

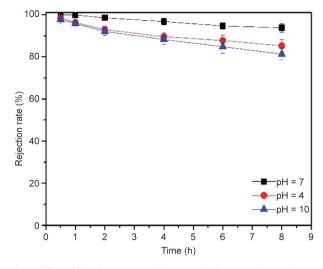


Fig. 7. Effect of initial pH on Cs rejection rate by the composite membrane.

hollow-fiber composite membrane [15,24]. Furthermore, CuFC can decompose in alkaline solution [15,24].

3.5. Effect of competing cations

The chloride salts of K⁺ and Na⁺ were selected to test the role of competing cations in the Cs rejection rate using composite membranes. As shown in Fig. 8, the rejection rate of the prepared composite membrane was high (99%), but the rejection rate of the pristine PVDF membrane was negligible. The membranes also showed a high rejection rate even after the addition of competing monovalent cations for 8 h. However, the rates decreased with an increase in the duration of the filtration time. Compared with Na⁺, K⁺ showed a greater detrimental effect on Cs rejection rate; this might be due to the fact that K⁺ has a similar hydration radius (0.331 nm) as Cs⁺ (0.329 nm), which could induce competition [3,21]. The Cs rejection rate decreased with an increase of filtration time (Fig. 6), indicating that physical interception by the membrane is not the primary removal mechanism for Cs. As shown in Fig. 8, the Cs rejection rates were not greatly affected by the presence of competing cations, and remained above 90% for the first 2 h of unsaturated adsorption. Adsorption saturation of Cs was gradually reached and the Cs rejection rate was reduced with an increase

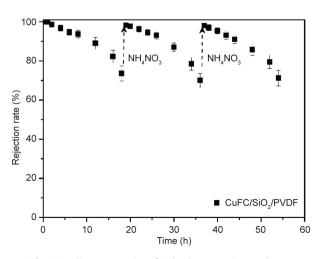


Fig. 6. Loading-regeneration of Cs by the composite membrane.

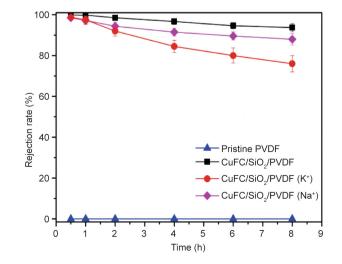


Fig. 8. Effects of competing cations on Cs rejection rate by the composite membrane.

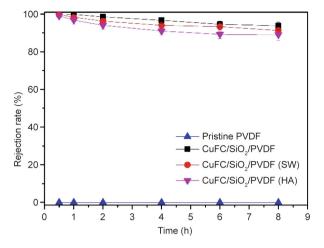


Fig. 9. Effect of organics on Cs rejection rate by the composite membrane.

of filtration time. Thus, the results show that adsorption by the modified membrane is the major mechanism for Cs removal.

3.6. Effects of organics

The effects of organics on Cs rejection rate using composite membrane filtration were tested in an HA solution and in SW; the results are shown in Fig. 9. The membrane continued to have a high Cs rejection rate (> 90%) in both solutions for 8 h. During this period, HA was deposited onto the membrane surface; this might have helped keep the rejection rate high due to size exclusion and Donnan exclusion [6]. Therefore, in addition to adsorption, size exclusion and Donnan exclusion on the membrane surface play an important role in Cs removal. It can be concluded that the composite membrane has excellent application potential for Cs removal.

4. Conclusions

In this work, a hollow-fiber composite membrane was prepared using the facile method of binding CuFC onto a PVDF membrane surface in order to remove Cs from water. SiO₂ NPs were used as an intermediate support layer, and chemical bonding of CuFC to the membrane surface occurred. The CuFC/SiO₂/PVDF hollowfiber composite membranes exhibited high selectivity toward Cs and membrane flux. The membrane was able to directly and quickly filter out Cs in water, with a rejection rate higher than 99%. Furthermore, Cs rejection rate could be restored to more than 98% using 5 mol·L⁻¹ NH₄NO₃. The rejection rates were slightly affected by the solution pH and by competing cations. In addition, the composite membrane demonstrated good selectivity for water with a low Cs concentration (100 μ g·L⁻¹), including SW and simulated water with HA. Overall, the functionalized composite membrane showed excellent potential for the removal of radionuclide Cs.

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Compliance with ethics guidelines

Shiyuan Ding, Lilan Zhang, Yang Li, and Li'an Hou declare that they have no conflicts of interest or financial conflicts to disclose.

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