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Green Production Technology of the Monomer of Nylon-6: Caprolactam Baoning Zong*, Bin Sun, Shibiao Cheng, Xuhong Mu, Keyong Yang, Junqi Zhao, Xiaoxin Zhang, Wei Wu

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ABSTRACT

After two decades' endeavor, the Research Institute of Petroleum Processing (RIPP) has successfully developed a green caprolactam (CPL) production technology. This technology is based on the integration of titanium silicate (TS)-1 zeolite with the slurry-bed reactor for the ammoximation of cyclohexanone, the integration of silicalite-1 zeolite with the moving-bed reactor for the gas-phase rearrangement of cyclohexanone oxime, and the integration of an amorphous nickel (Ni) catalyst with the magnetically stabilized bed reactor for the purification of caprolactam. The world's first industrial plant based on this green CPL production technology has been built and possesses a capacity of 200 kt·a⁻¹. Compared with existing technologies, the plant investment is pronouncedly reduced, and the nitrogen (N) atom utilization is drastically improved. The waste emission is reduced significantly; for example, no ammonium sulfate byproduct is produced. As a result, the price difference between CPL and benzene drops. In 2015, the capacity of the green CPL production technology reached 3×10^6 t·a⁻¹, making China the world's largest CPL producer, with a global market share exceeding 50%.

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1. Introduction

In the future, sustainable development of the chemical industry must be built on a foundation of green chemistry and green engineering, and the general concept must change from one of polluting first and treating later, to one of eliminating pollution at the source. The criteria of green chemistry are: to achieve overall atom economy of a reaction—that is, every atom of the source materials enters into the product, thus producing no waste or byproducts—and to avoid the use of toxic or harmful raw materials, catalysts, or solvents. In brief, the target of green chemistry is to produce chemicals in a clean manner that does not pollute the environment at any point in the entire life cycle.

Caprolactam (CPL), as the monomer for nylon-6 fiber and engineering plastics, is an important basic organic chemical that is widely used in textile, automobile, electronics, and other industries. In 2015, CPL consumption amounted to about 3×10^6 t in China and about 6×10^6 t around the world [1]. Two decades ago, CPL consumption in China relied almost completely on importation; therefore, China Petrochemical Corporation (Sinopec) invested 9 billion CNY to introduce three CPL production plants with a total capacity of 150 kt·a⁻¹. However, commercial CPL production technology has disadvantages such as low production capacity, high investment and production cost, and high waste emission, which are far from the criteria of green chemistry; thus, CPL production demands process improvement. This review outlines the green CPL production technology that was developed by the Research Institute of Petroleum Processing (RIPP) in recent years.

2. Existing CPL production technology

Of all the basic organic chemicals, CPL has the most complex production process, and the purity standard of its product is the most stringent. The existing CPL production technology was developed in the 1980s; it mainly consists of the hydrogenation of benzene to cyclohexane, the oxidation of cyclohexane to cyclohexanone, the

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oximation of cyclohexanone by hydroxylamine to cyclohexanone oxime, the liquid-phase Beckmann rearrangement of cyclohexanone oxime to CPL, and a multi-step purification process. The first key technology in this production is the oximation of cyclohexanone by hydroxylamine to cyclohexanone oxime (Table 1), which involves the oxidation of ammonia to NO_x, the absorption and reduction of NO_x to hydroxylamine, and the reaction of hydroxylamine and cyclohexanone to produce cyclohexanone oxime. This process has the shortcomings of high consumption of the noble metal catalyst, use of the highly toxic NO_x, and only 60% utilization of ammonia. The second key technology is the liquid-phase Beckmann rearrangement of cyclohexanone oxime to CPL (Table 1). In this process, fuming sulfuric acid is used as the solvent and the catalyst, resulting in the production of a large amount of low-value ammonium sulfate. The third key technology is the CPL purification process, which involves hydrogenation, distillation, and ion-exchange steps to reduce the impurity content to less than 5 µg·g⁻¹. Thus, in addition to its complexity, the existing CPL production technology has harsh reaction conditions involving corrosive and highly toxic NO_x and SO_x, and its utilization of nitrogen (N) is only 60%. According to the statistical data of a 50 kt·a⁻¹ CPL production plant using the existing technology, the production of one ton of CPL discharges 5000 m³ of waste gas, 5 t of waste water, and 0.5 t of waste residue, in addition to producing 1.6 t of low-value ammonium sulfate. Therefore, there is a high demand for the development of a green CPL production technology.

3. The green CPL production technology

The green CPL production technology developed by RIPP comprises the integration of titanium silicate (TS)-1 zeolite with the slurry-bed reactor for the ammoximation of cyclohexanone, the integration of silicalite-1 zeolite with the moving-bed reactor for the gas-phase Beckmann rearrangement of cyclohexanone oxime, and the integration of amorphous nickel (Ni) catalyst with the magnetically stabilized bed reactor for the purification of CPL.

3.1. Integration of TS-1 zeolite with a slurry-bed reactor for the ammoximation of cyclohexanone

In the 1980s, EniChem Company developed TS-1 zeolite to catalyze the one-pot reaction of cyclohexanone, ammonia, and hydrogen peroxide to produce cyclohexanone oxime, as shown in Table 1, with an impressive selectivity. The advantages of this reaction are its highly simplified process, mild reaction conditions, and high atom economy, with water being the only byproduct. Subsequently, a 12 kt·a⁻¹ industrial demonstration was accomplished in 1995. The technology employed spherical catalysts with a diameter of 20 µm and tanks-in-series slurry-bed reactors. The cyclohexanone conversion was no less than 99.9%, the cyclohexanone oxime selectivity was no less than 99.3%, and the hydrogen peroxide utilization was around 90%. Based on this technology, Sumitomo Chemical Co., Ltd. built a 65 kt·a⁻¹ CPL production plant in 2003.

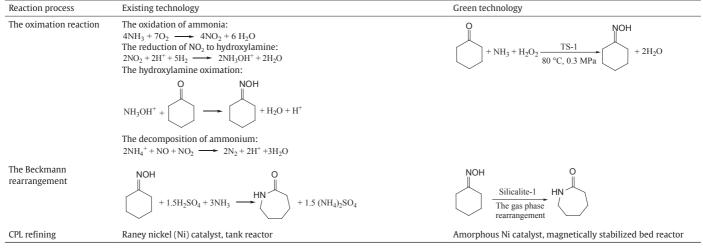
During the same period, RIPP developed a cyclohexanone ammoximation technology by integrating micro-sized hollow TS-1 zeolite with a slurry-bed reactor fitted with a membrane separation component. Fig. 1 provides a schematic diagram of the ammoximation of cyclohexanone based on this technology. RIPP began its investigation of this new technology in 1995 and achieved commercialization success in 2003.

To solve the problems of the poor preparation reproducibility of TS-1 zeolite and of its unstable activity and selectivity in the reaction, a state-of-the-art catalyst-preparation strategy was developed by combining hydrothermal synthesis with secondary structural modification, giving rise to the micro-sized hollow TS-1 zeolite [2]. A 100 t-a⁻¹ production unit of the micro-sized hollow TS-1 zeolite was built at Sinopec Catalyst Co., Ltd. in 2002.

The cyclohexanone ammoximation technology developed by RIPP has two highlights. The first is the use of the micro-sized hollow TS-1 zeolite as the catalyst and the integration of a membrane separation component into the slurry-bed reactor. Directly synthesizing the micro-sized hollow TS-1 zeolite as the catalyst not only removes the need for the catalyst-forming process, but also enables a more effective utilization of the active centers. Moreover, with the aid of the membrane separation component, the micro-sized hollow TS-1 zeolite can be uninterruptedly separated and recycled. The second highlight is the improvement in controlling catalyst loss and in catalyst regeneration. It is known that silicon (Si) tends to dissolve from the TS-1 zeolite because the ammoximation of cyclohexanone is an alkalescent system. The loss of Si reduces the activity of the catalyst. The dissolved Si also blocks the separation membrane. Therefore, controlling the loss of Si is the key to the stable, safe, and long-term operation of the production plant. The new technology effectively suppresses the loss of Si based on a proprietary method and thus prolongs the lifetime of the catalyst. At the same time, it improves the catalyst renewability and reduces catalyst consump-

Table 1

The existing CPL production technolog	y and the green CF	^P L production technology.
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tion [3,4]. For the cyclohexanone ammoximation technology developed by RIPP, the cyclohexanone conversion was more than 99.9%, the cyclohexanone oxime selectivity was more than 99.3%, and the hydrogen peroxide and ammonia utilization was around 90% and 100%, respectively.

Compared with the existing technology, the new technology of integrating micro-sized hollow TS-1 zeolite with a slurry-bed reactor fitted with a membrane separation component markedly simplifies the cyclohexanone ammoximation process. Moreover, it improves the utilization of N from 60% to nearly 100%, decreases the plant investment by more than 70%, eliminates the production or use of corrosive NO_x, and discharges almost no waste. As a result, the production cost of cyclohexanone oxime is reduced by 800 CNY·t⁻¹. Fig. 2 shows the 200 kt·a⁻¹ cyclohexanone oxime industrial production unit that was established based on this technology.

3.2. Integration of silicalite-1 zeolite with a moving-bed reactor for the gas-phase Beckmann rearrangement of cyclohexanone oxime to CPL

The processes for the Beckmann rearrangement of cyclohexanone oxime to CPL can be categorized into two types: the liquid-phase and the gas-phase Beckmann rearrangement. The liquid-phase Beckmann rearrangement process adopts fuming sulfuric acid as the solvent and catalyst. It requires a large amount of ammonia to neutralize the reaction system after the rearrangement, and produces 1.6 t of low-value ammonium sulfate per ton of CPL. In addition, the fuming sulfuric acid severely corrodes the equipment and pollutes the environment. Furthermore, the product purification and refining process of the liquid-phase Beckmann rearrangement is tedious; it generally involves rearrangement neutralization, extraction and steam-stripping of ammonium sulfate, benzene extraction, water extraction, ion exchange, hydrogenation, triple-effect evaporation, and distillation. Finally, because of the demand for fuming sulfuric

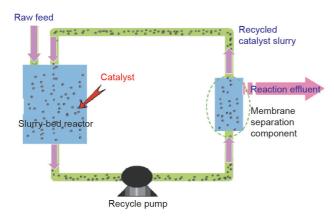


Fig. 1. Schematic diagram of the ammoximation of cyclohexanone.



Fig. 2. The 200 kt·a⁻¹ cyclohexanone oxime industrial production unit.

acid and liquid ammonia in the liquid-phase Beckmann rearrangement, CPL production enterprises usually have to build supporting workshops for sulfuric acid, liquid ammonia, and ammonium sulfate, resulting in high fixed investment and labor costs.

In 2010, an industrial demonstration began of the gas-phase Beckmann rearrangement of cyclohexanone oxime that was developed by RIPP [5,6]. Fig. 3 shows a gas-phase Beckmann rearrangement industrial demonstration unit of 10 kt·a⁻¹, and Fig. 4 shows a crystallization purification industrial demonstration unit of 10 kt·a⁻¹. The gas-phase Beckmann rearrangement technology has three highlights: ① the improved synthesis and molding technology of silicalite-1 zeolite; ② using the radial moving bed as the reactor; and ③ the crystallization purification of the product. Fig. 5 presents the industrial demonstration results. The cyclohexanone oxime conversion was higher than 99.9% and the CPL selectivity was around 96.5%. Compared with the existing liquid-phase Beckmann rearrangement process, the new technology does not produce ammonium sulfate, thus essentially achieving "zero" pollutant emission and reducing the production cost by about 1000 CNY·t⁻¹.

3.3. Integration of amorphous Ni catalyst with a magnetically stabilized bed for hydrofining CPL

As mentioned above, the purity standard of CPL is the most stringent out of all the basic organic chemicals. The impurity content in CPL should be less than $5 \,\mu g \cdot g^{-1}$ in order to ensure the desired



Fig. 3. A 10 $\rm kt\text{-}a^{-1}$ industrial demonstration unit of the gas-phase Beckmann rearrangement.



Fig. 4. A 10 kt·a⁻¹ crystallization purification industrial demonstration unit.

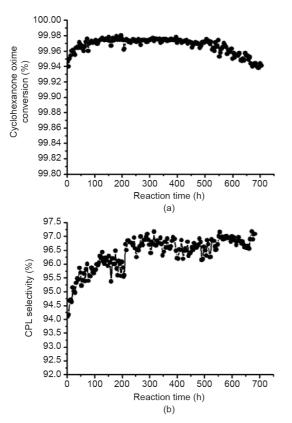


Fig. 5. Industrial demonstration results of the gas-phase Beckmann rearrangement. (a) Cyclohexanone oxime conversion; (b) CPL selectivity.

pigmenting and spinning properties. However, the impurities bear physical and chemical properties that are similar to those of CPL, and cannot be removed through extraction or distillation. The existing production technology uses a Raney Ni catalyst and tank reactor for the hydrofining of CPL in order to extend the boiling point gap between the impurities and CPL, followed by removal of the impurities by distillation. The process for this hydrofining technology is complex, its catalyst consumption is high, its hydrogenation efficiency is low, and the catalyst must be separated from CPL by filtration. We found that replacing the Raney Ni catalyst with an amorphous Ni catalyst significantly enhances the hydrogenation activity. Integrating an amorphous Ni catalyst with the magnetically stabilized bed reactor intensifies the CPL purification process, improves the quality of CPL, increases the CPL yield, and favorably reduces the operation cost.

3.3.1. Amorphous Ni catalyst

An amorphous alloy has a unique structure that features shortrange order and long-range disorder; thus, the alloy exhibits excellent electromagnetic, mechanical, and wear-resisting performance. However, an amorphous alloy is non-equilibrium metastable in thermodynamics. Its poor thermal stability and small specific surface area severely limit its application in catalytic reactions. We introduced large-radius rare-earth atoms into amorphous Ni to retard the migration of the Ni atoms, thus elevating the crystallization temperature by 160 °C. We also developed a pore-creating method by adding aluminum (Al) first, and then leaching it out with alkali, thus improving the specific surface area by two orders of magnitude. Various additives can easily be introduced to the amorphous alloy to meet the requirements of different types of hydrogenation reactions, including the hydrofining of CPL [7]. The magnetism of an amorphous Ni alloy favorably satisfies the requirements of the solid catalysts demanded by the magnetically stabilized bed reactor. The magnetically stabilized bed reactor facilitates a high-speed operation because the external magnetic field can effectively prevent fine particles from leaving the reactor. Therefore, integrating an amorphous Ni catalyst with the magnetically stabilized bed reactor for the hydrofining of CPL takes full advantage of this new catalytic material and this new type of reactor [8].

We also systematically studied the influence of the cooling speed of amorphous Ni and iron (Fe) alloys on their catalytic performances. We discovered that the scientific key to a good catalytic performance of an amorphous alloy lies in the fact that quenching reduces the coordination number and changes the distance between the metal atoms [9]. Therefore, we devised a new strategy for finely regulating the catalytic performance of the metal catalysts [10–12]. Amorphous metal alloy catalysts also exhibited excellent activity and selectivity in benzene partial hydrogenation [13], methanation [14], biomass conversion [15,16], and so on.

3.3.2. Magnetically stabilized bed reactor

The magnetically stabilized bed reactor, which combines the advantages of the fixed-bed reactor and the fluidized-bed reactor, is a special type of reactor that is operated in a uniform magnetic field with magnetic particles as the solid phase [17]. In the 1980s, the magnetically stabilized bed was an important basic research project of the Exxon Corporation, although so far it has not been commercialized by the Exxon Corporation because of the lack of proper magnetic catalysts and reaction systems. In 1999, RIPP conducted bench-scale studies on the hydrofining of CPL using the magnetically stabilized bed reactor and an amorphous Ni catalyst. These studies showed that conducting the hydrofining of a CPL aqueous solution in the magnetically stabilized bed reactor drastically increased the potassium permanganate (PM) value, from 60 s to 3000 s. Note that the PM value is one of the quality indexes for CPL, with a higher PM value indicating fewer unsaturated impurities. By comparison, in the tank reactor, the PM value only increased to 300 s. In addition, in the magnetically stabilized bed reactor, the lifetime of the amorphous Ni catalyst was longer than 1350 h. These results showed the prospect for the industrial application of the magnetically stabilized bed reactor.

Prior to industrial application, it was essential to figure out the hydrodynamic characteristics of the magnetically stabilized bed, because of its distinct differences from the fixed-bed reactor and the ordinary fluidized-bed reactor. In 2000, RIPP established a coldmold experimental unit of the magnetically stabilized bed reactor (Fig. 6), through which the hydrodynamic characteristics, the mass transfer properties, and the reaction kinetics of the liquid-solid twophase magnetically stabilized bed were systematically studied. The effects of the operation parameters, including the magnetic field intensity, the physicochemical properties of the catalyst, and the fluid velocity on the bed structure, were identified, thus implementing effective control of the catalyst by the magnetic field and enabling the establishment of the mathematical model of the magnetically stabilized bed reactor and the operation phase diagram for catalysts of different sizes. All these findings provided a solid scientific basis for the commercialization of the magnetically stabilized bed reactor.

We found that producing a uniform magnetic field is one of the key factors in the industrial amplification of the magnetically stabilized bed reactor. It was discovered that the magnetic field strength increased gradually along the radial direction after amplification. When the diameter of the coils was enlarged to 770 mm, the magnetic field strength at the inner surface of the coils became 15% higher than that at the center of the coils. In order to improve the uniformity of the magnetic field, we designed and developed magnetic retainer internals with different spacings and achieved a uniform radial magnetic field distribution. In addition, since the heat generated by the working coils increased the temperature, a forced-cooling method was adopted to implement the long-term, safe, and stable operation of the coils.

In 2001, Sinopec Baling Company established a 6 kt·a⁻¹ CPL hydrofining demonstration unit (Fig. 7). The results showed that the PM value of the 30% CPL aqueous solution increased from 40–60 s to 2000–4000 s after hydrofining using the magnetically stabilized bed reactor. In addition, the hydrogenation result was significantly better than that of the existing industrial stirred-tank process, with the PM value increasing to 200–400 s after hydrofining. The conditions for the hydrofining of CPL on the magnetically stabilized bed reactor are as follows: temperature of 80–100 °C, pressure of 0.4– 0.9 MPa, space velocity of 30–50 h⁻¹, and magnetic field strength of 15–35 kA·m⁻¹. The lifetime of the amorphous alloy catalyst reached 3500 h [8].

To extend the application of the magnetically stabilized bed reactor, we designed and synthesized a series of iron-based magnetic catalysts, which showed excellent catalytic performance in the Fischer-Tropsch synthesis reaction [18–24]. We also synthesized magnetic resins with embedded nano-sized iron oxides as the magnetic cores, with which a magnetic palladium catalyst and a magnetic solid-acid catalyst were fabricated. On the magnetic stabilized bed reactor, these magnetic catalysts were highly effective for hydrofining [25], impurity removal from ethylene [26], oligomerization of light olefins [27], and etherification of fluid catalytic cracking (FCC) light



Fig. 6. Experimental apparatus of the magnetically stabilized bed reactor.



Fig. 7. The 6 kt·a⁻¹ demonstration unit of the magnetically stabilized bed reactor.

gasoline [28]. A magnetic separator was also designed and used in the Fischer-Tropsch synthesis process, and a process package of industrial equipment with a capacity of millions of tons per year has been designed.

3.3.3. Industrial application of the magnetically stabilized bed for CPL hydrofining

In 2003, Sinopec Shijiazhuang Chemical Fiber Co., Ltd. built a 65 kt-a⁻¹ CPL industrial plant, and realized the industrial application of the magnetically stabilized bed reactor for the first time. In 2009, the company built a new magnetically stabilized bed hydrofining plant with a scale of 100 kt-a⁻¹, which began stable operation (Fig. 8). The unit can be conveniently started and shut down. Table 2 provides the long-term operation results. The PM value of the 30% CPL aqueous solution increased from 100 s to 4000 s after hydrofining on the magnetically stabilized bed reactor, while the catalyst consumption was reduced by 50%.

4. Conclusions

After two decades' endeavor, RIPP successfully developed a green production technology for CPL, the monomer of nylon-6, by integrating new catalytic materials, new chemical engineering, and new reaction pathways. This technology greatly simplifies the CPL production process. As a result, plant investment is reduced by 70%



Fig. 8. The 100 kt·a⁻¹ CPL purification magnetically stabilized bed reactor unit.

Table 2

Comparison between magnetically stabilized bed and tank reactors for the purification of CPL.

Items		Magnetically stabilized bed reactor	Tank reactor
Reaction conditions	Temperature (°C)	80	90
	Pressure (MPa)	0.7	0.7
	Liquid hourly space velocity (h^{-1})	30	2
	Hydrogen/liquid rate (v/v)	2.0	2.0
	Magnetic field intensity (kA·m ⁻¹)	20	_
PM value of the feed CPL solution (s)		100	100
PM value of the hydrotreated CPL solution (s)		4000	800
Catalyst consumption $(kg \cdot t_{CPL}^{-1})$		0.1	0.2

and the utilization of N is increased from less than 60% to nearly 100%. The waste emission of this technology is close to zero, with no byproduct production of ammonium sulfate. Hence, the price difference between CPL and benzene drops from 20 000 CNY·t⁻¹ to 5000 CNY·t⁻¹. The world's first industrial plant using this technology was built, with a capacity of 200 kt·a⁻¹. In 2015, China's CPL capacity based on this green production technology reached 3×10^6 t·a⁻¹, giving China a global market share that exceeds 50%, and making it the world's largest CPL producer—a huge leap from China's original position of relying almost totally on CPL importation. This green CPL production technology forms a foundation for new industries with an output of 50 billion CNY, thus not only producing great economic and social benefits, but also setting a good example of green chemical engineering.

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Compliance with ethics guidelines

Baoning Zong, Bin Sun, Shibiao Cheng, Xuhong Mu, Keyong Yang, Junqi Zhao, Xiaoxin Zhang, and Wei Wu declare that they have no conflict of interest or financial conflicts to disclose.

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